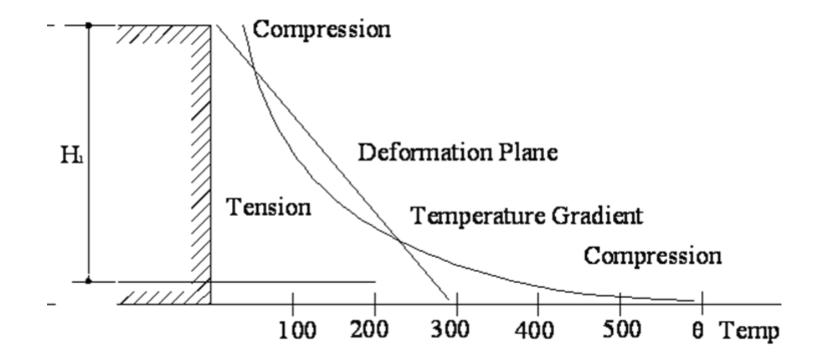
# Full-scale Fire Tests on Hollowcore Floor System

Colin Bailey: University of Manchester

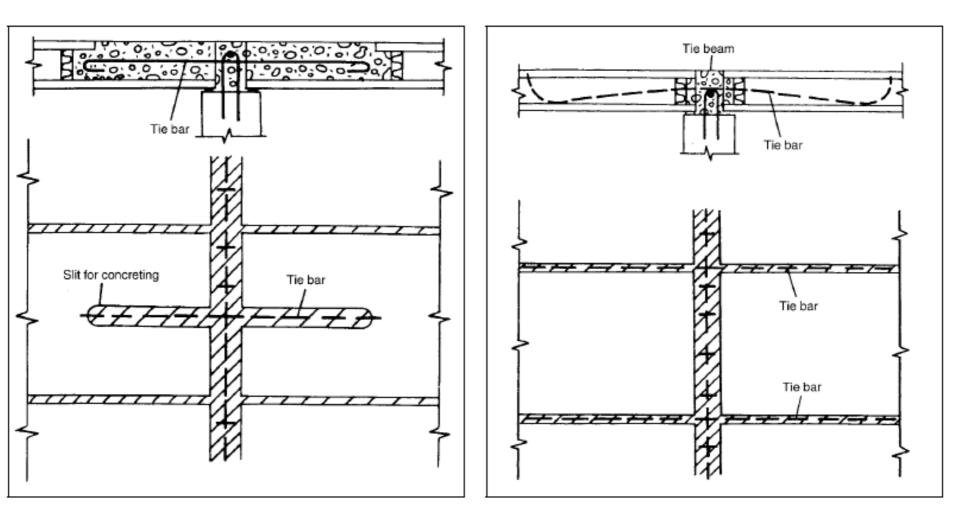
## Why?

Evidence from small-scale tests of possible premature shear failure



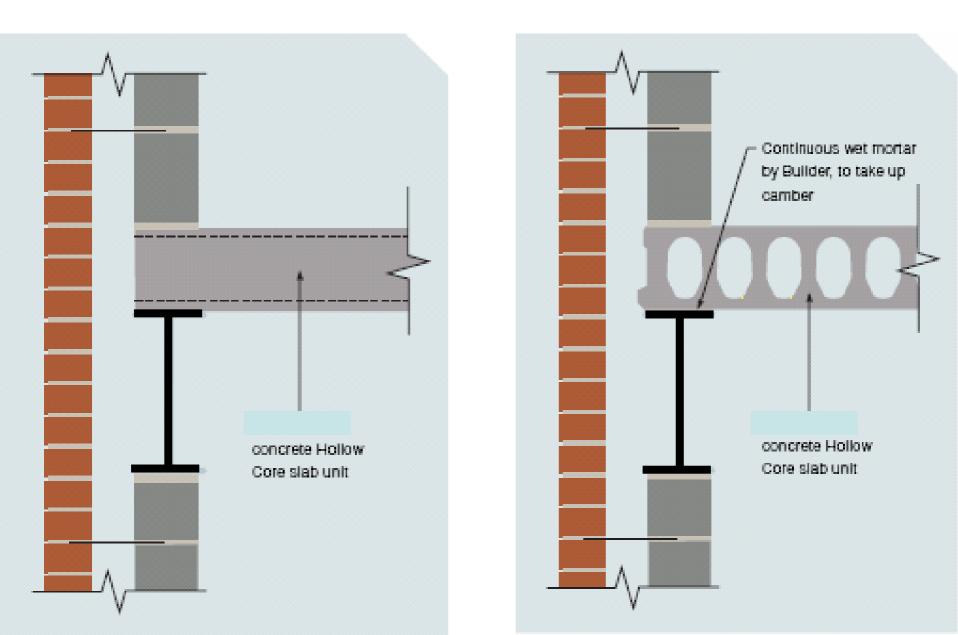
Evidence from real fires suggests that hollowcore floors have a inherent FR

*Pragmatic approach*: Provided units are tied (together with a peripheral tie) then shear failure should not occur



## Class 2A buildings

But !



## **Class 2A Buildings**

Offices, hotels, and residential buildings not exceeding 4 storeys

Industrial buildings not exceeding 3 storeys

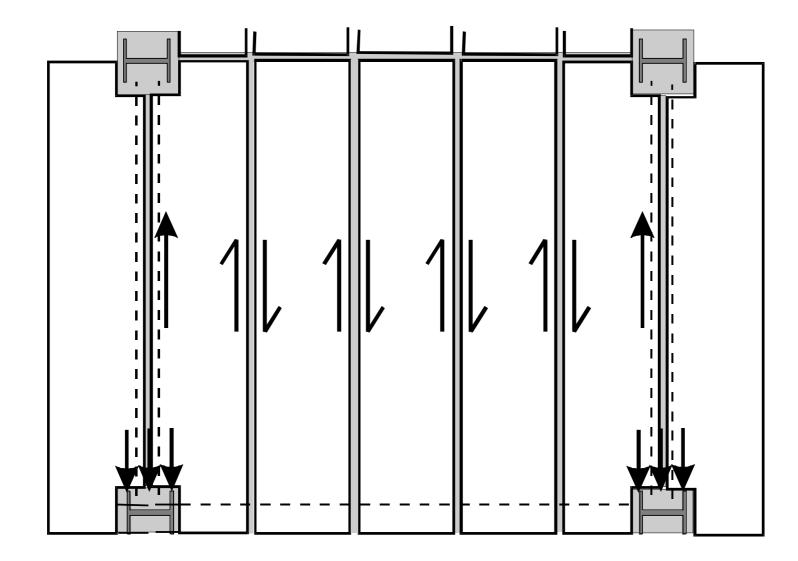
### Class 2B Buildings

Offices, hotels, and residential buildings greater than 4 storeys but less than 15 storeys.

Hospitals not exceeding 3 storeys

## Class 3 Buildings

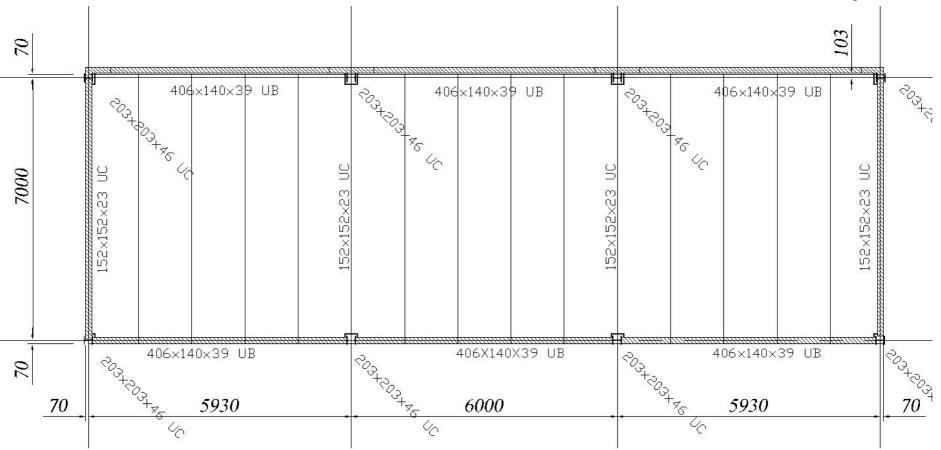
Buildings not defined as Class 2A or 2B



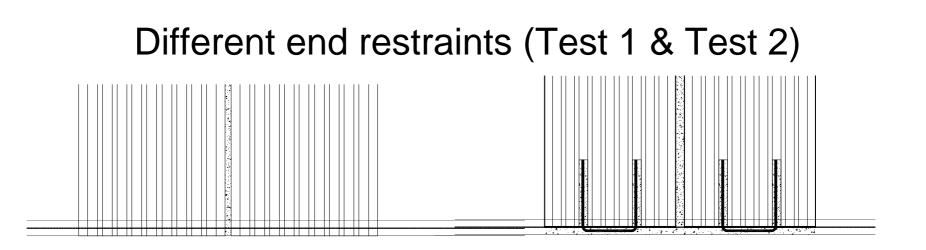
Thermal expansion of units is restrained provided the columns are tied and the tie beams do not expand more than the units.

# Test Structure: 7.02m×17.76m (internal plan dimensions) ×3.6m height

15 units 1.2m widex200mm deep







Test 1

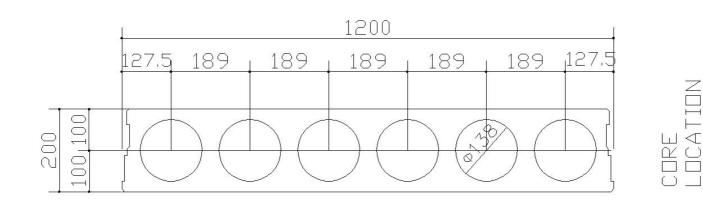
Test 2

No additional 'fixity'

Class 2A

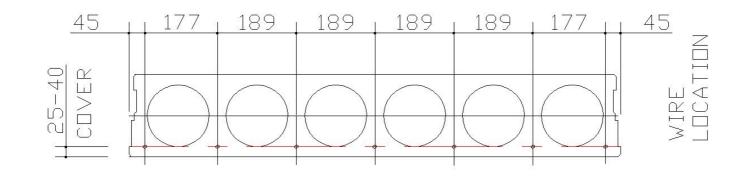
(Generally under 4 stories)

T12 u-bars per unit were placed around 19mm dia stud. Class 2B



Cover to strands = 25 mm to obtain 60 mins FR

7No. 12.5 mm strand per unit



Limestone aggregate -M/C = 2.8% by weight



Test 1: Units sit directly on steel beams and grout placed between units and around columns



## Test 1

Grout placed between units and around column

# Exposed steel requires protection

### Tie beam

#### Wall offset column line

#### Wall on column line

Fire Protection:

15mm Lafarge fire board60mins FR in standard test.

## Fire Load:

Aim: to try and follow standard fire curve upto 60 mins.

Used Annex A from BSEN1991-1-2

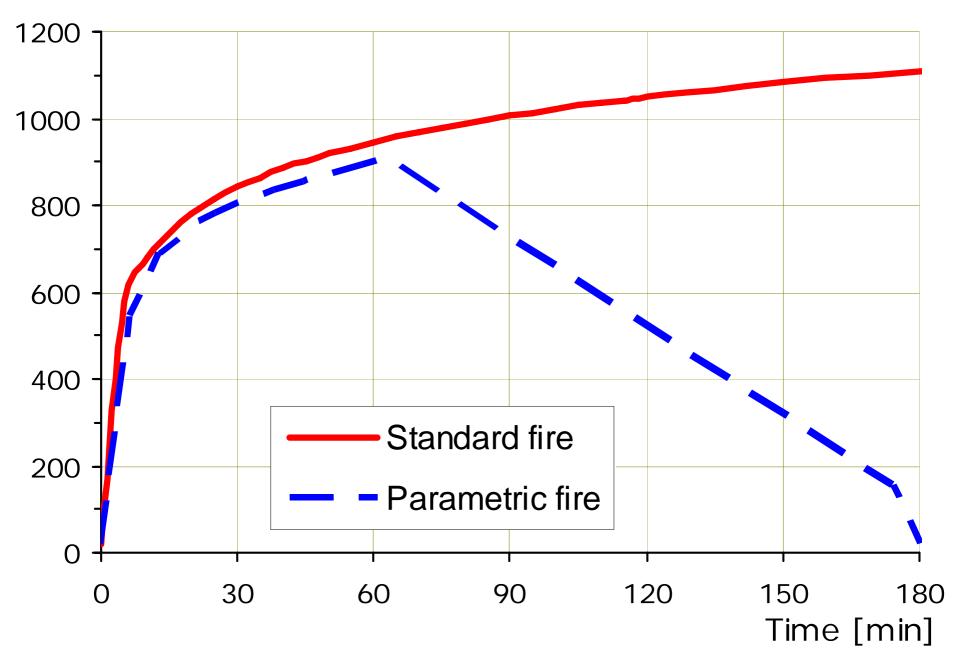
Office fire load =  $511MJ/m^2$ 

UK NA Office load =  $570MJ/m^2$ 

 $\therefore$  32.5kg wood/m<sup>2</sup> used.



```
Temperature [°C]
```

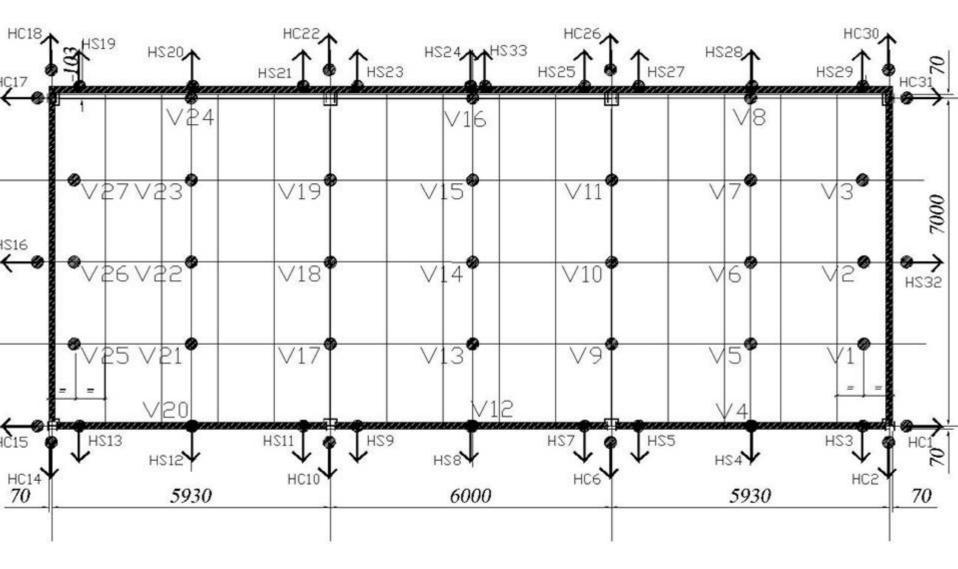


3 openings 2.2m×16m high

Increase in ventilation will increase temp & decrease duration



Total load =  $7.67 \text{ kN/m}^2$  (Applied =  $4.71 \text{ kN/m}^2$ ) Load Ratios: 0.34 bending; 0.26 shear.



Horizontal movement measured at 33 locations Vertical displacement measured at 27 locations





Temperature measurements: per test

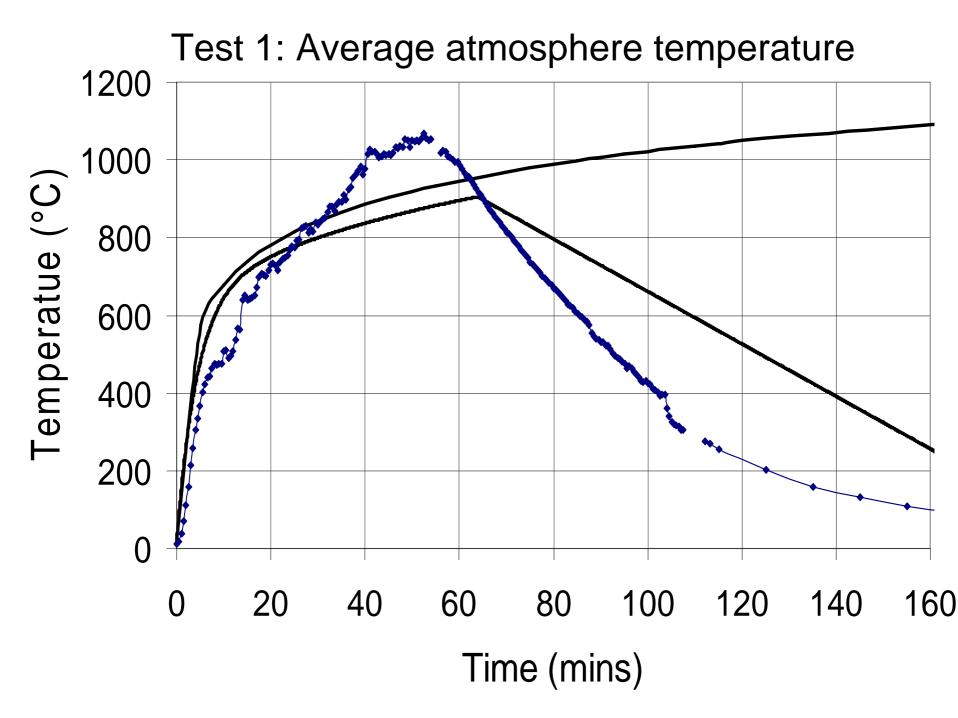
- 24 atmosphere temperature measurements
- 90 beam temperature measurements
- 140 slab temperature measurements

#### A total of 628 data points were measured

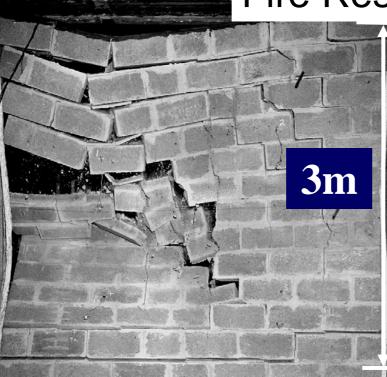




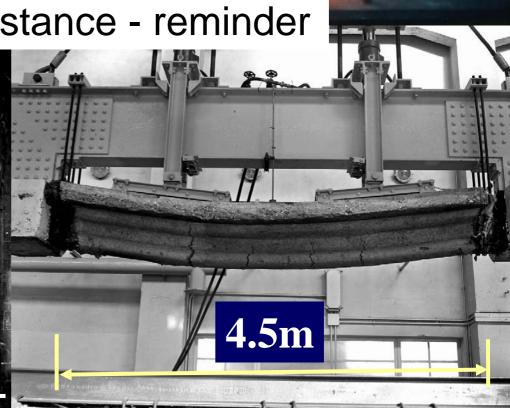




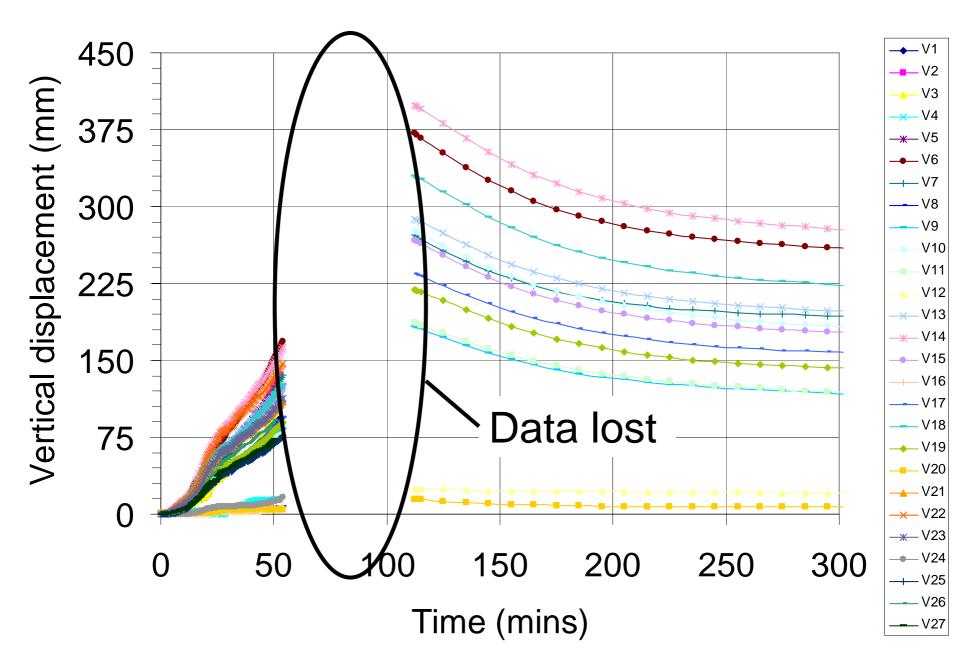
### Fire Resistance - reminder



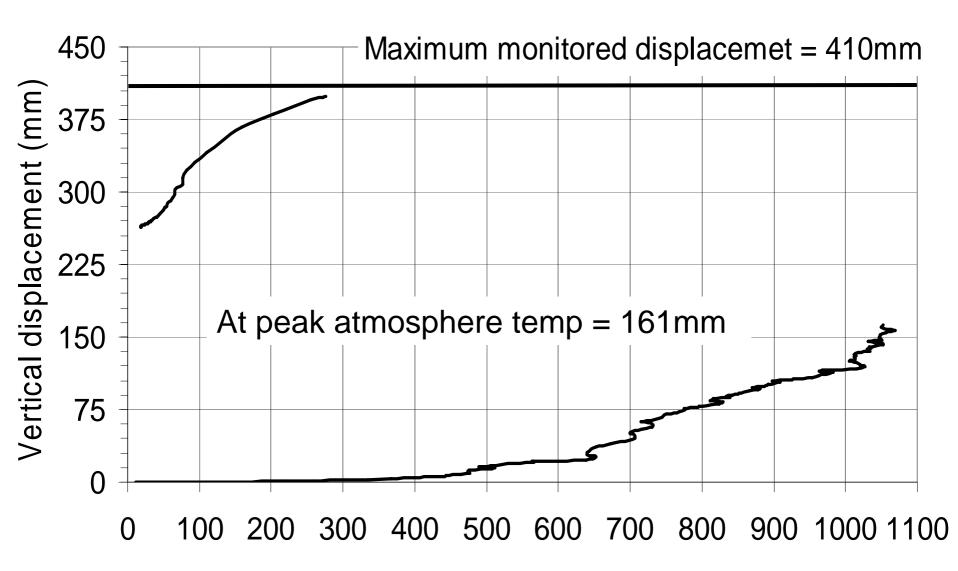
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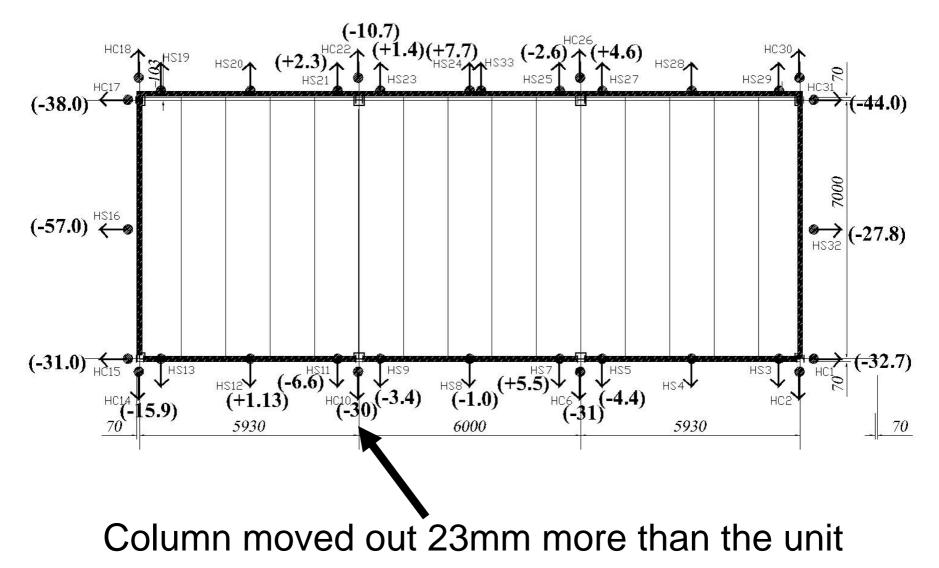




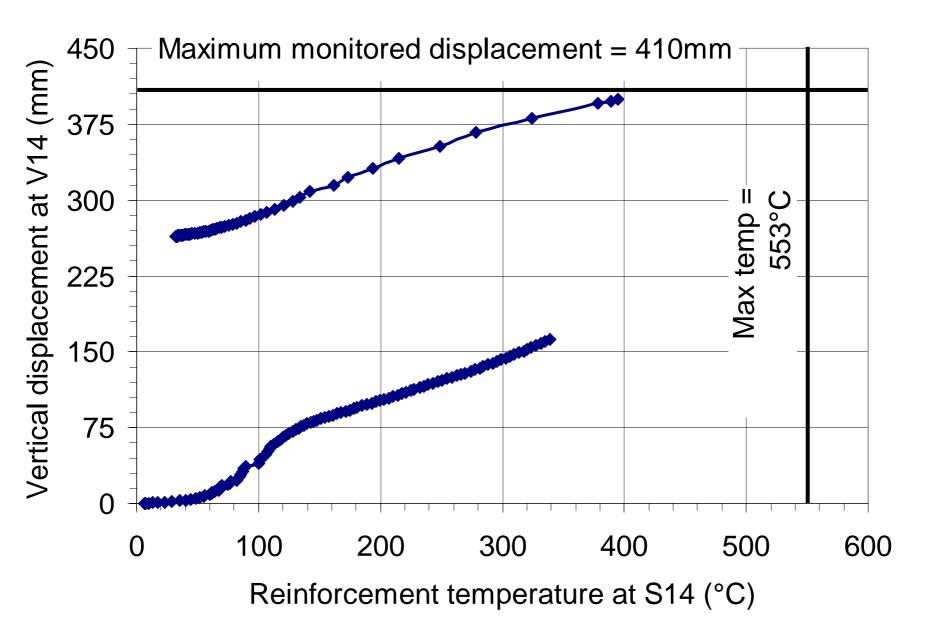
Average atmosphere temperature (°C)



# Horizontal displacements at 54 mins (1053°C atmosphere temp)



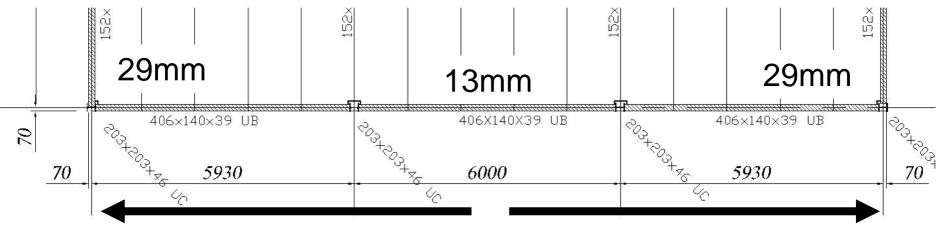




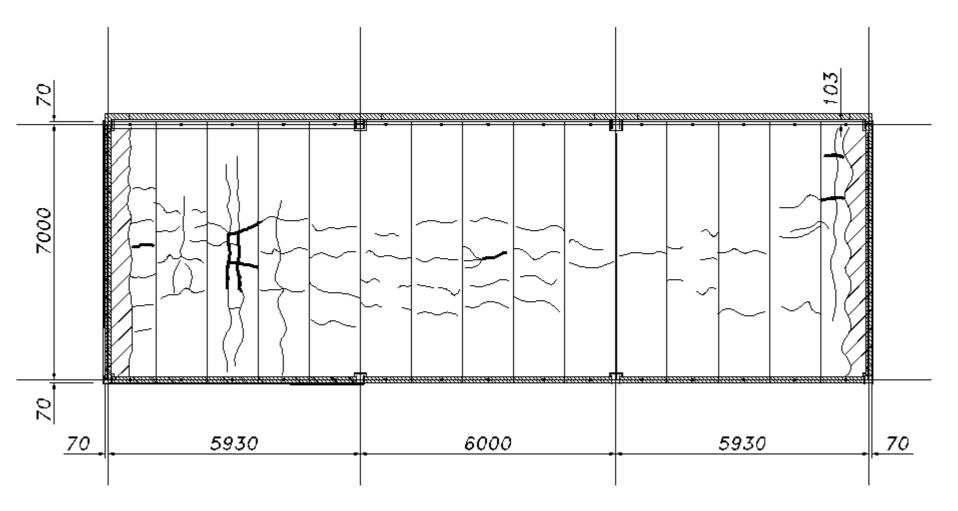


- Design to BSEN1992-1-2 Maximum strand temp = 553°C
- Flexural capacity = 39.7kNm
- Applied load = 54.8kNm





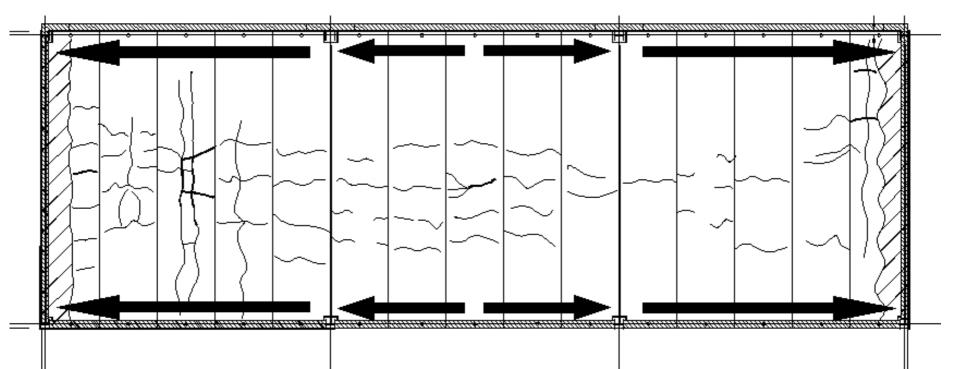
Residual slippage increased towards ends





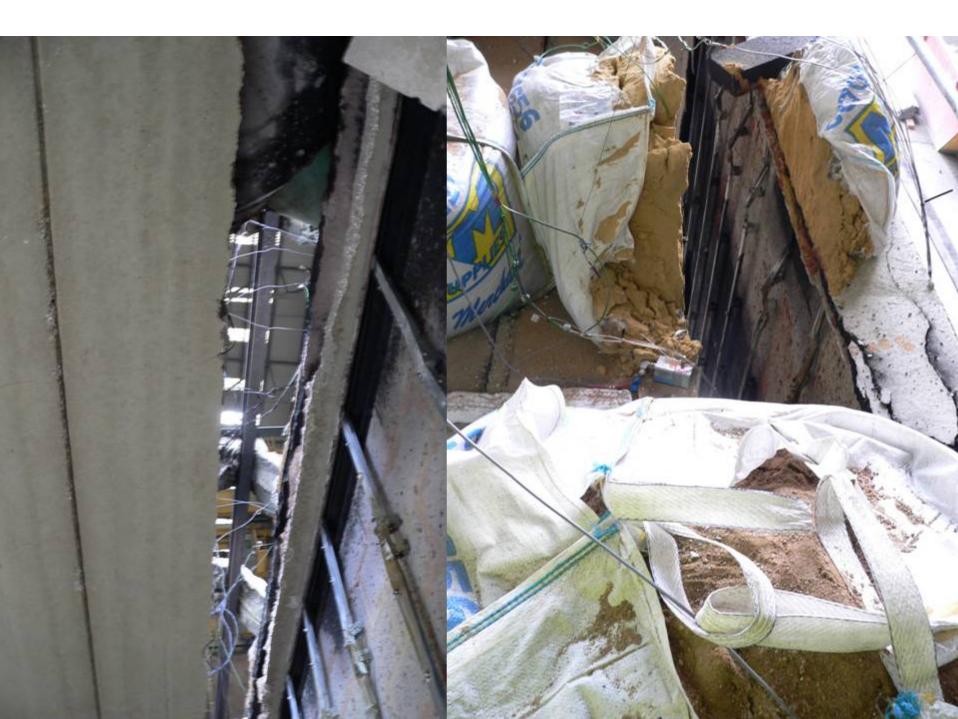
#### Test 1

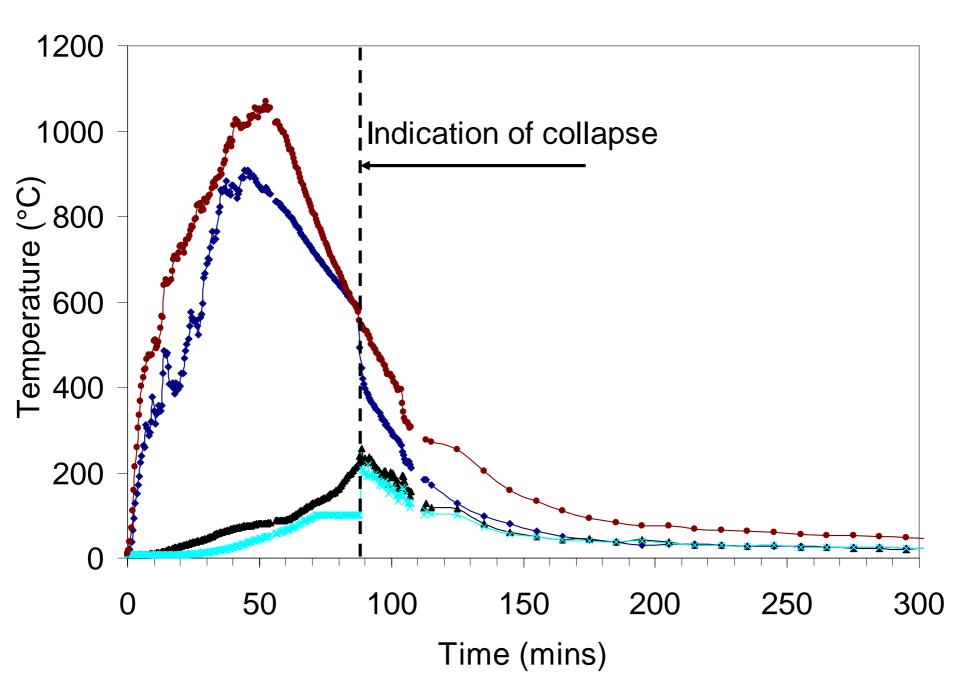
# No significant spalling





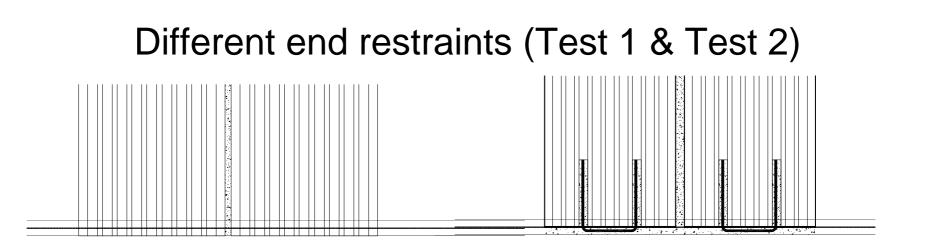








#### Test 2: Different end conditions



Test 1

Test 2

No additional 'fixity'

Class 2A

(Generally under 4 stories)

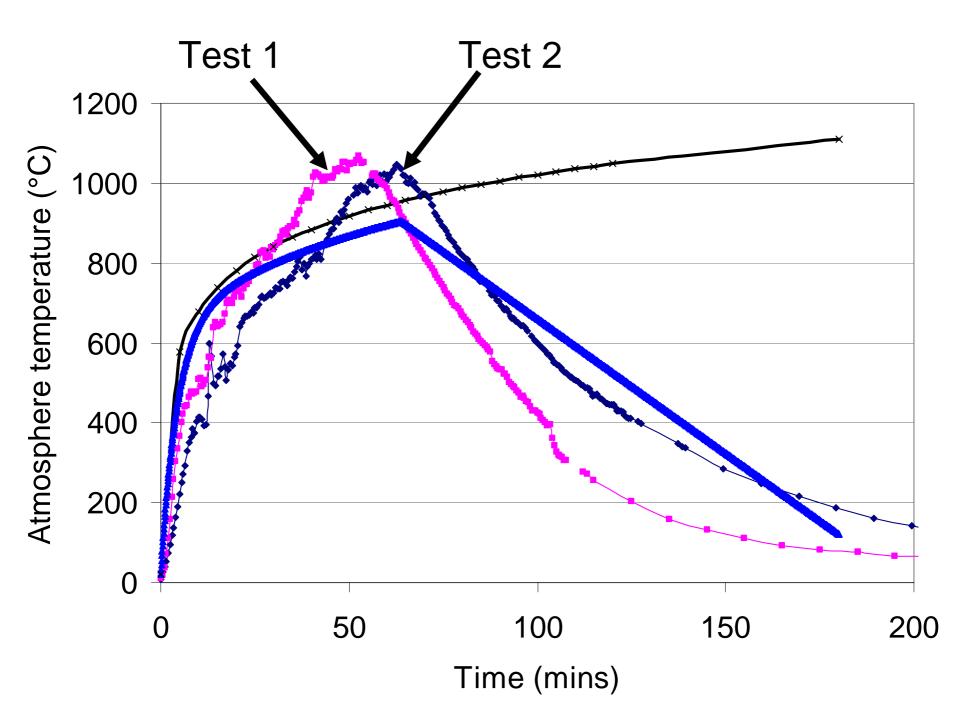
T12 u-bars per unit were placed arround 19mm dia stud. Class 2B

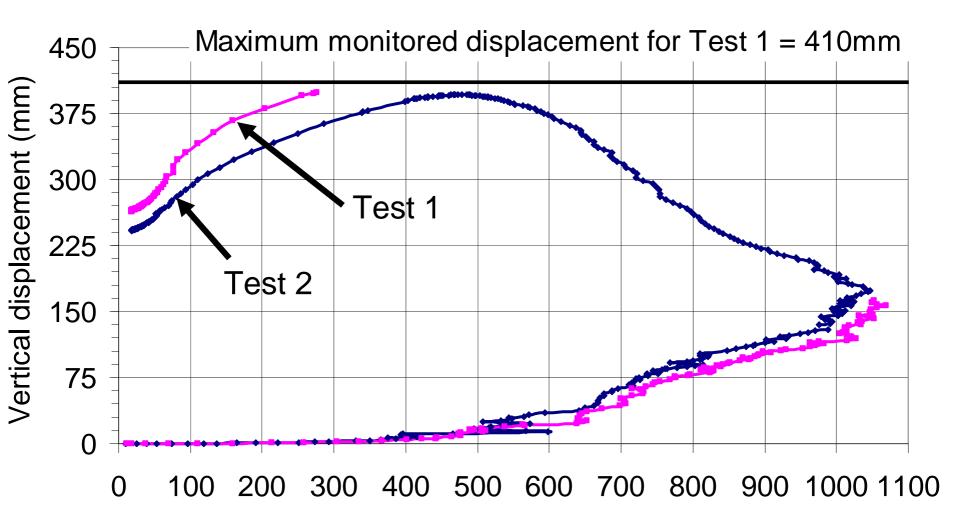


## Test 2 : Additional reinforcement







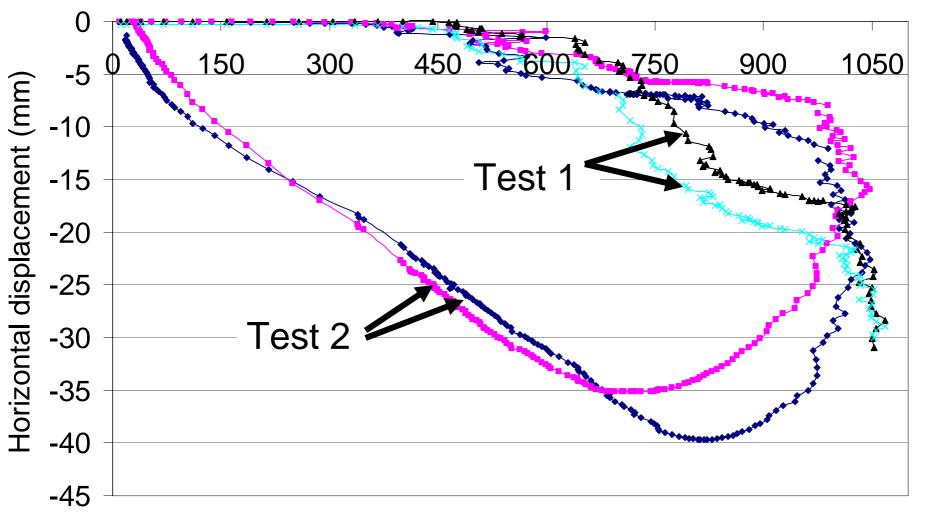


Average atmosphere temperature (°C)

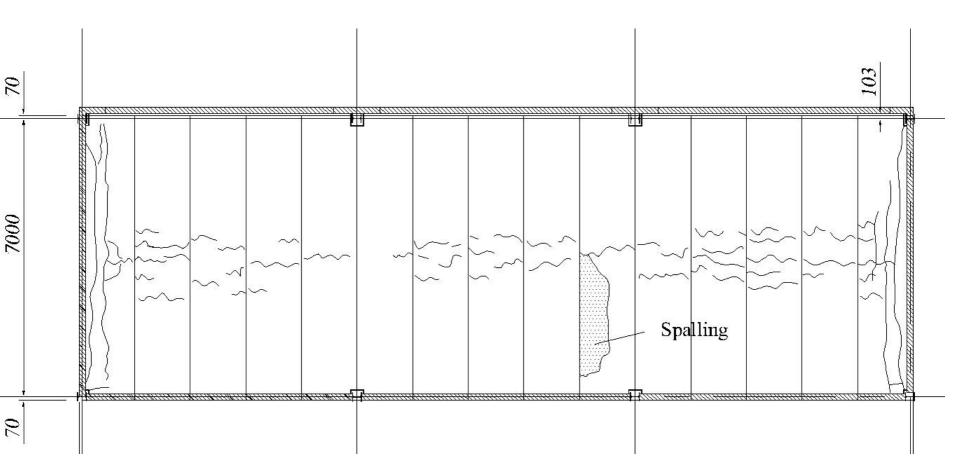
#### Column pushed out

1 de la

#### Column displacement



Average atmosphere temperature (°C)









Additional bars kept unit in place

(Time of fracture can be obtained from data) Fracture of end units:

#### Test 1: 87mins (576°C) & 103 mins (394 °C)

## Test 2: 76mins (870°C) & 95mins (645°C)



#### Conclusions (1)

•System performed well during the heating phase, under a very severe (unrealistic ?) fire.

•The system supported the applied load during the cooling phase (even though this was ignored during the design)

•Test 1 and Test 2 had similar performance (except for the end units).

•There was evidence of a lateral compressive strip forming enhancing flexural and shear capacity.

#### Conclusions (2)

• No significant spalling occurred.

•The parametric curve produced lower temps during the heating phase and should be addressed.

•Although the applied load was higher than the assumed office load the LRs of 0.34 and 0.26 were low. A range of LRs should be considered.

Acknowledgements

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### Thank you